"SHARING TO BE BETTER" "SHARING TO BE SAFER"



Under the direction of OLF, a joint industry task force of Operator and Drilling Contractor personnel has been formed to recommend ways to reduce the number and potential severity of well control events on the NCS.

One team recommendation was communicating actual well control incidents that have recently occurred on the NCS so lessons are shared and understood.

This is the **second** in a series of five case histories. This incident highlights the importance of following procedures, attention to detail and quality control of calculations performed on the rig

Please take some time at your next safety meeting to review this case history and discuss the questions raised during the presentation.

It is hoped that sharing of incidents is helpful and any feedback is welcome.



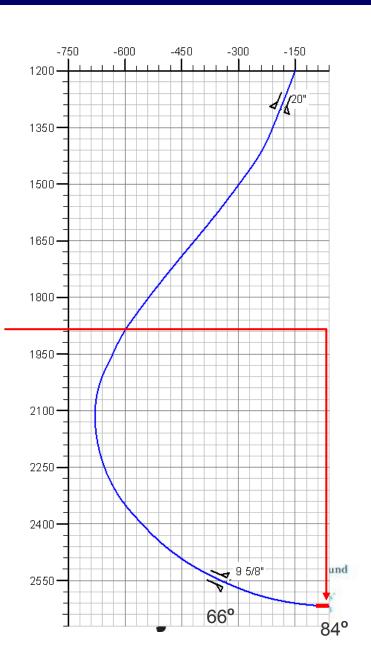
Offshore Semisub Rig

Well Control Incident



Drilling 8 1/2" section

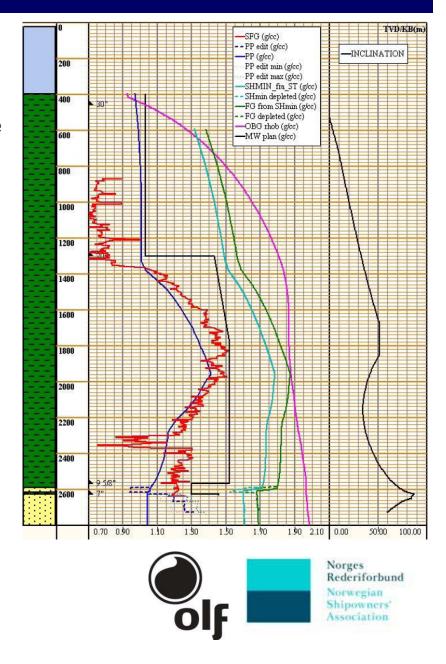
- Water depth: 395 m
- 9 5/8" casing shoe inclination: 66 deg
- FIT: 1.61 sg EMW
- Mud weight: 1.30 sg OBM
- 8 ¹/₂" open hole length: 350 m
- 8 ¹/₂" section TD inclination: 84 deg
- 8 ¹/₂" section TD: 6 mMD into permeable formation



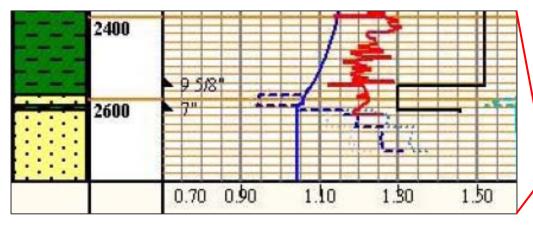
- During circulation at TD the Data Operator (mud logger) was preparing a swab calculation before POOH
- He contacted the Wellsite Geologist to ask which pore pressure to use in the calculation. The Wellsite Geologist was busy describing cuttings and told the Data Operator (mud logger) to look in the drilling program to find the pore pressure

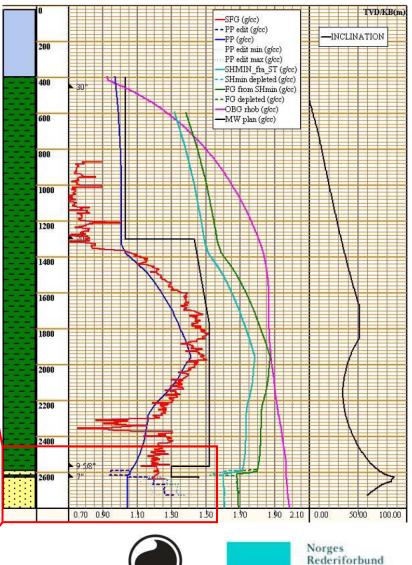


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- During circulation at TD the Data Operator (mud logger) was preparing a swab calculation before POOH
- He contacted the Wellsite Geologist to ask which pore pressure to use in the calculation. The Wellsite Geologist was busy describing cuttings and told the Data Operator (mud logger) to look in the drilling program to find the pore pressure
- The Data Operator read of the value 1.06 sg from the pore pressure plot. He added a safety margin of 0.02 sg and used **1.08 sg** as input to the swab calculation





Norwegian Shipowners' Association

SWAB TRI	PPING S	PEED CA	LCULATIONS		
	POOH				
DATE:	28-mar-10				
STRING:	BHA #7				
TOTAL DEPTH:	3445				
MUDWEIGHT:	1.3	SG			
LAST FIT:	1.61	SG			
LAST Pore P:	1.08	SG			
Max ECD	1.41	SG			
Heave effect :	0.1	m/sec			
BIT DEPTH			Running spe	ed w/ heave	
meters	m/sec	sec/std	m/sec	sec/std	m/hr
3500	0.78	37	0.68	43	2448
3000	0.8	36	0.70	41	2520
2500	0.85	34	0.75	39	2700
2000	0.89	33	0.79	37	2844
1500	0.91	32	0.81	36	2916
1000	0.93	31	0.83	35	2988

Would you have questioned this swab calculation?



SWAB TRI	PPING S	PEED CA	LCULATIONS		
	POOH				
DATE:	28-mar-10				
STRING:	BHA #7				
TOTAL DEPTH:	3445				
MUDWEIGHT:	1.3	SG			
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Would you have questioned this swab calculation?

- Very high pulling speed



SWAB TRI	PPING S	PEED CA	LCULATIONS		
	POOH				
DATE:	28-mar-10				
STRING:	BHA #7				
TOTAL DEPTH:	3445				
MUDWEIGHT:	1.3	SG			
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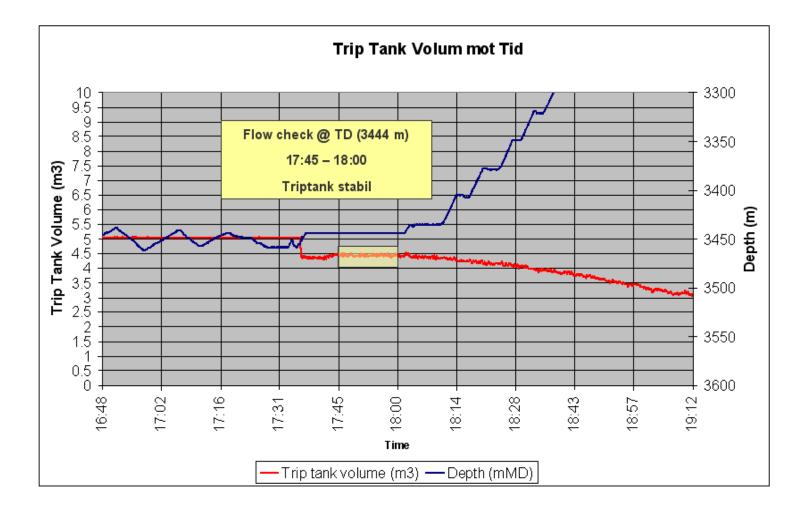
Would you have questioned this swab calculation?

- Very high pulling speed

- The Drilling Supervisor did not quality check the input values and results of the calculation.
- Nobody (Drilling Supervisor / Toolpusher / Driller) reacted on the fast pulling speed

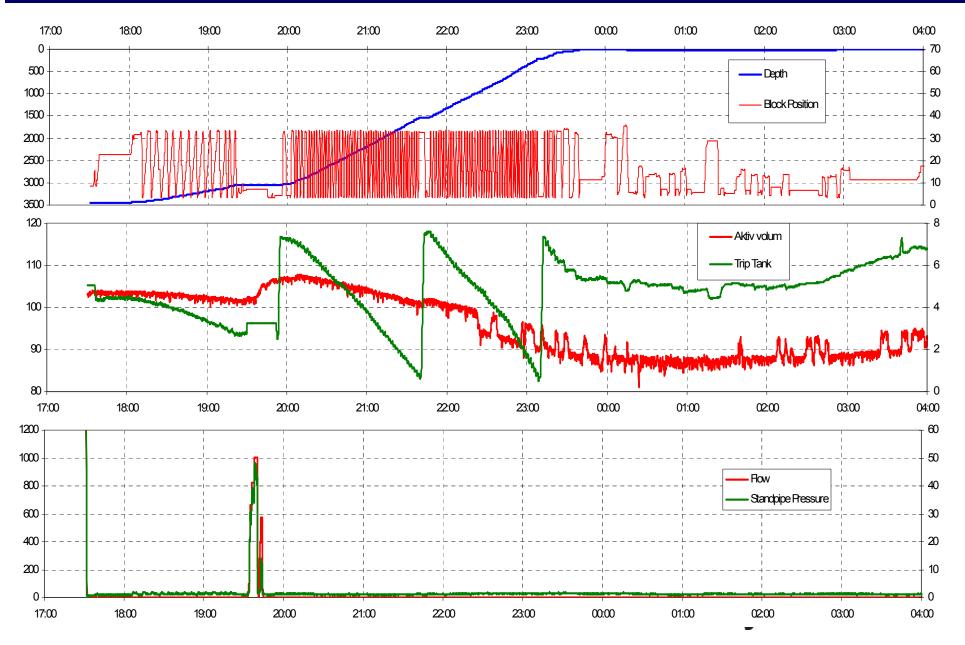


Flow check at TD – well stable





POOH – Do you see anything you would have done differently?



This is the Data Operators (mud logger) trip sheet during the trip out of hole

TRIP TANK THOUGHTS:

What is the accuracy of the trip tank on <u>YOUR</u> rig?

When was the trip tank last calibrated on <u>YOUR</u> rig?



Stands in hole	Π m ³	Active	Transfer	Diff + / - m ³	Theo. Volume	Gain / Loss m ³	Cum. diff m ³	time	0.40	0.20	- 0.00	- 0.20	- 0.40	- 0.60	- 0.80	- 1.00	1.20
114	4.44			0.00	0.000	0.00	0.00			11	4	'	'		'		
111	4.09			-0.35	-0.424	0.07	0.07			11	1 🔳	_					
108	3.81			-0.28	-0.424	0.14	0.22			10	8						

After pulling 6 stands wet in open hole

220 Itr gain (cumulative from TD)

Would you have reacted on this observation?



Stands in hole		Active	Transfer	Diff + / - m ³		Gain / Loss m ³	m ³	time	-0.40	0.20	0.00	0*0	- 0.60	- 0.80	- 1.00	L 1.20
114	4.44			0.00	0.000	0.00	0.00			114	L					
111	4.09			-0.35	-0.424	0.07	0.07			111						
108	3.81			-0.28	-0.424	0.14	0.22			108						
105	3.31			-0.50	-0.424	-0.08	0.14			105						
102	2.90			-0.41	-0.424	0.01	0.16			102						

Inside 9 5/8" casing shoe

160 Itr gain (cumulative from TD)

Would you have reacted on this observation?



	Stands in hole	TT m ³	Active	Transfer	Diff + / - m ³	Theo. Volume	Gain / Loss m ³	Cum. diff m ³	time	-0.40	0.20	0.00 -	- 0.20	0.40	- 0.60	- 0.80	1.20
[114	4.44			0.00	0.000	0.00	0.00			11	4					
[111	4.09			-0.35	-0.424	0.07	0.07			11	1 📕	_				
[108	3.81			-0.28	-0.424	0.14	0.22			10	8					
[105	3.31			-0.50	-0.424	-0.08	0.14			10	<u>ا</u>					
[102	2.90			-0.41	-0.424	0.01	0.16			10	2					
[99	7.15		-4.49	-0.24	-0.424	0.18	0.34			9	9			_		
	96	7.01			-0.14	-0.424	0.28	0.62			9	6					

After pulling 6 stands inside 9 5/8" casing

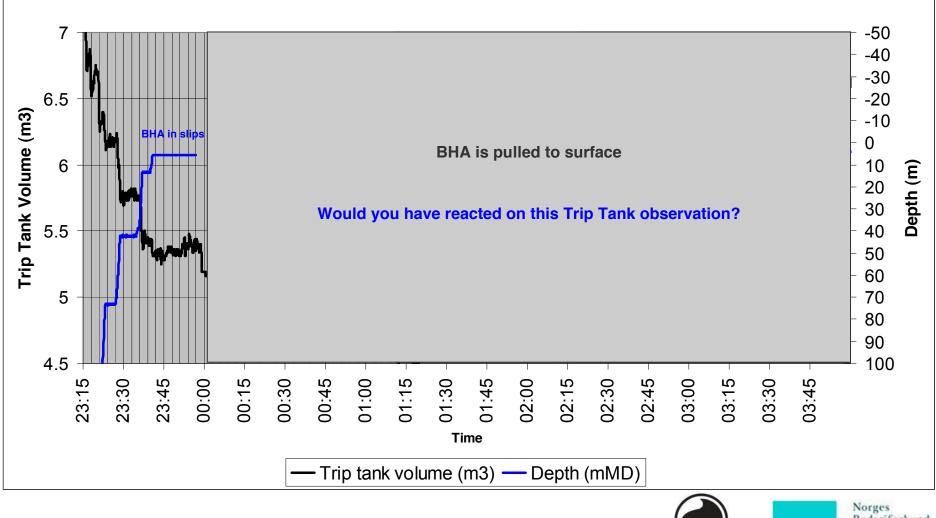
620 Itr gain (cumulative from TD)

Would you have reacted on this observation?



Stands in hole	Π m ³	Active	Transfer	Diff + / - m ³	Theo. Volume	Gain / Loss m ³	m ³		time	T -0.40	-0.20	0.00	0.20	0.40	0.80	8
114	4.44			0.00	0.000	0.00	0.00			L I	11	4				
111	4.09			-0.35	-0.424	0.07	0.07				11		_			
108	3.81			-0.28	-0.424	0.14	0.22				10	8				
105	3.31			-0.50	-0.424	-0.08	0.14				10	15 - C				
102	2.90			-0.41	-0.424	0.01	0.16				10	¹²				
99	7.15		-4.49	-0.24	-0.424	0.18	0.34				9	9				
96	7.01			-0.14	-0.424	0.28	0.62				9	6				
93	6.58			-0.43	-0.424	-0.01	0.62				9	3				
88	5.90			-0.68	-0.706	0.03	0.64				8	8				
83	5.26			-0.64	-0.706	0.07	0.71				8	3				_
78	4.74			-0.52	-0.706	0.19	0.90				7	78				
73	4.10			-0.64	-0.706	0.07	0.96				7	3				
68	3.33			-0.77	-0.706	-0.06	0.90				6	36 -				
63	2.62			-0.71	-0.706	0.00	0.90				6	3				
58	1.94			-0.68	-0.706	0.03	0.92				5	8				
53	1.30			-0.64	-0.706	0.07	0.99				5	3				
48	7.45		-7.00	-0.85	-0.706	-0.14	0.84				r d	8				1
43	6.63			-0.82	-0.706	-0.11	0.73				1	3				
38	5.79			-0.84	-0.706	-0.13	0.60				1	8			_	
33	5.15			-0.64	-0.706	0.07	0.66				3	33				
28	4.58			-0.57	-0.706	0.14	0.80				2	28				
23	3.83			-0.75	-0.706	-0.04	0.76				2	23				
18	3.19			-0.64	-0.706	0.07	0.82				1	8				
13	2.48			-0.71	-0.706	0.00	0.82	No flow check before			1	3				
8	1.63			-0.85	-0.706	-0.14	0.68					8				
3	0.93			-0.70	-0.706	0.01	0.68	BHA pulled through BC	אכ			3				
0	0.51			-0.42	-0.424	0.00	0.69					• -				
-3												-3 [
-6												-6]				

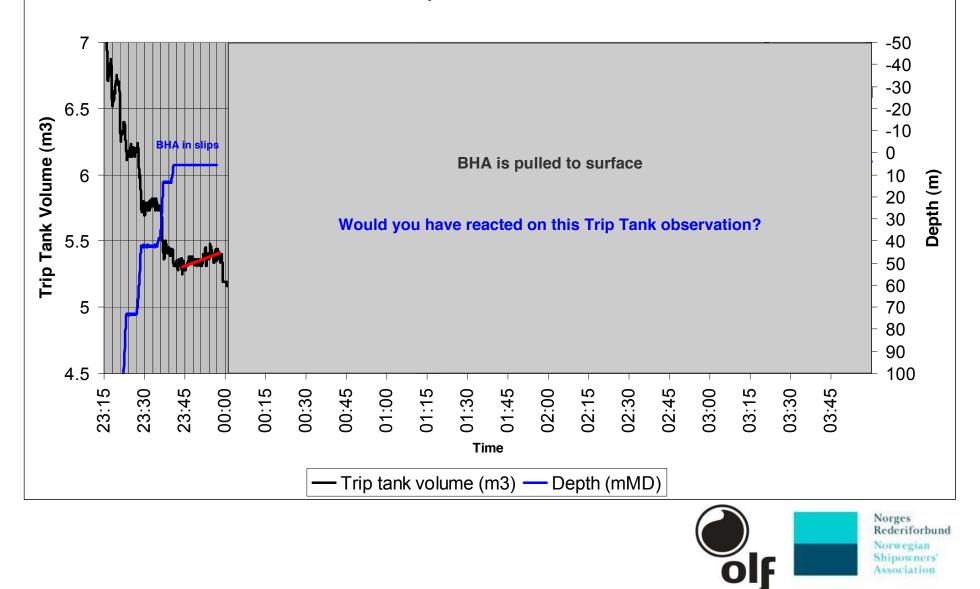




Trip Tank Volum mot Tid



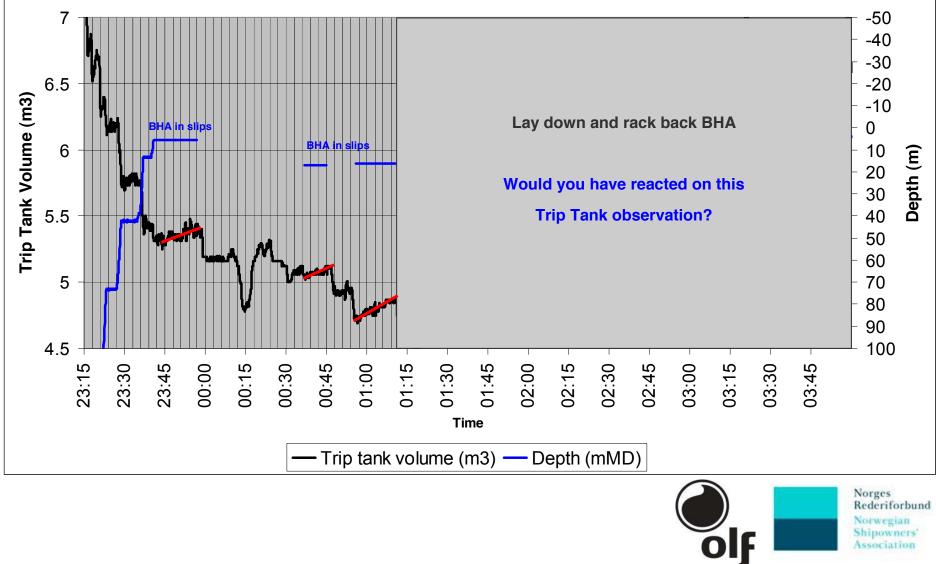
Trip Tank Volum mot Tid





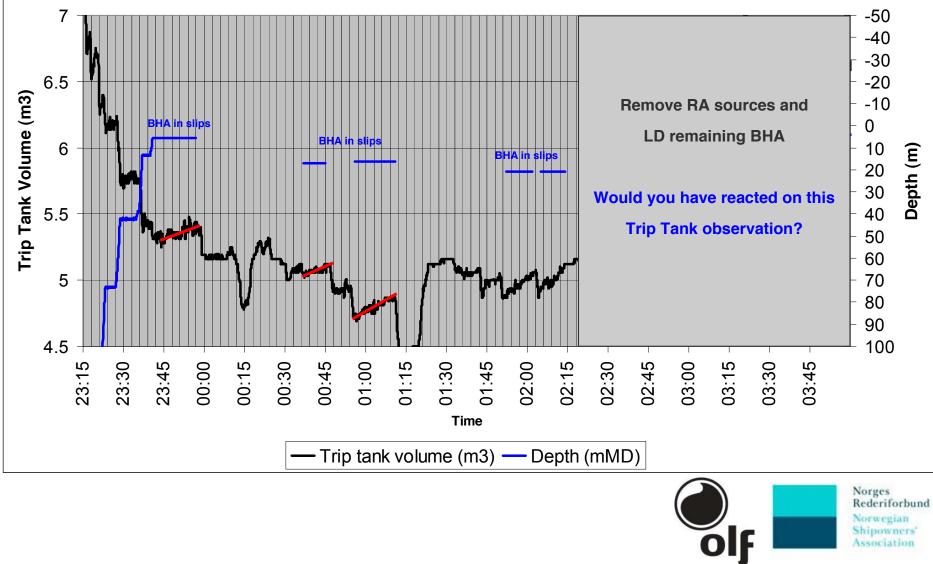
Trip Tank Volum mot Tid

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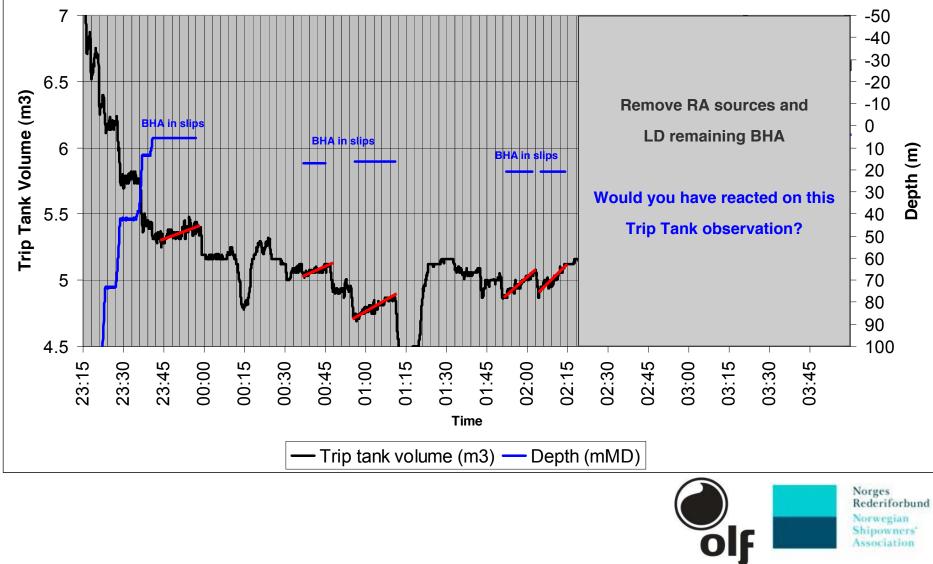
Shipowners Association

Trip Tank Volum mot Tid

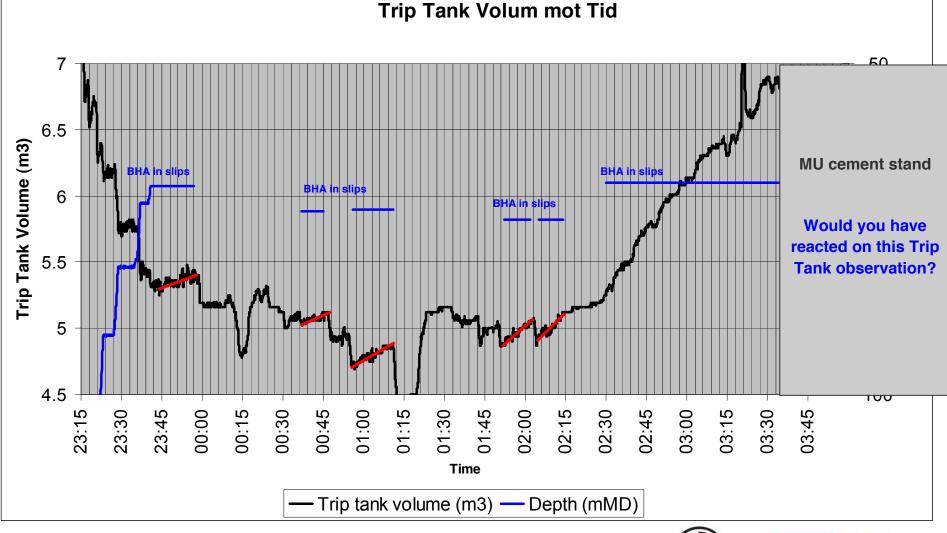


Shipowners Association

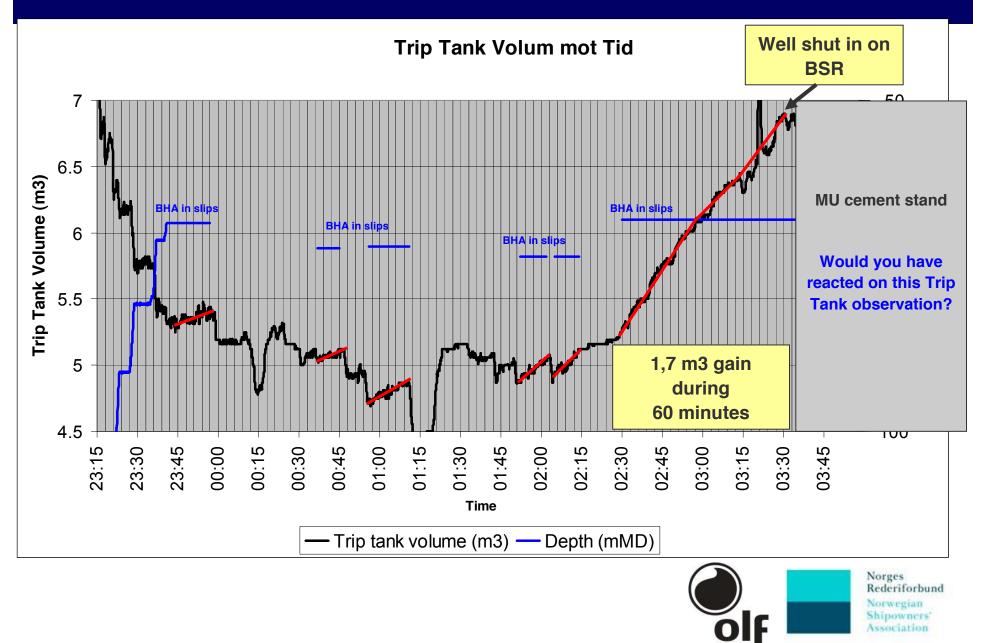
Trip Tank Volum mot Tid



Shipowners Association







CONCLUSION

- A kick has been taken during tripping out of hole and not discovered before out of hole.
- Well shut in on Blind shear ram.
- SICP=6,6 bar
- Discuss how you would have secured well?
 - Key info:
 - Drilled 6 m permeable formation
 - 1.30 SG OBM in well
 - Influx volume approx 2 m3
 - FIT on 9 5/8" shoe 1.61 SG (2560 m TVD).
- DIRECT CAUSE: SWABBING



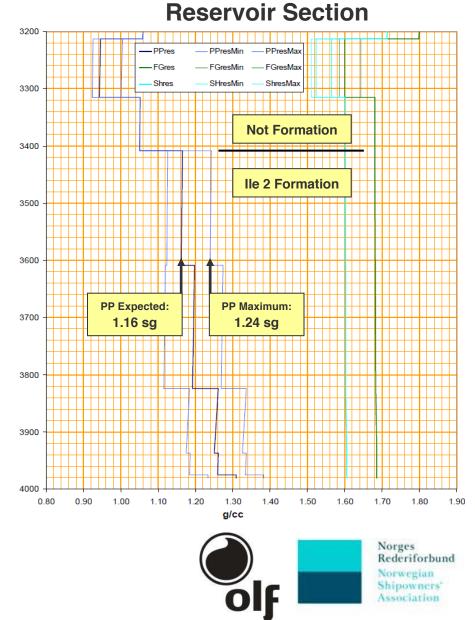
How primary barrier (fluid column) was regained

- •RIH with bullheading assmebly to above BOP
- •Drilling riser displaced to 1.54 sg OBM
- Cross circulated down kill and up choke lines with 1.54 OBM
 - ✓Flow checked well on trip tank well stable
- Open BSR and RIH with bullheading assembly to 700 m
 - ✓ Attempted to fracture permeable formation
 - ✓ not able to break down formation limited by FIT at 9 5/8" casing shoe
 - ✓ Displaced well to 1.54 sg OBM well stable
- RIH to 1000 m and displaced well to 1.52 sg OMB
 - ✓ Observed gas in return
 - ✓Well stable
- RIH and repeated well displacement to 1.52 sg OBM at 1500, 2200, 3150 m
 - ✓No gas observed well stable



Root causes

- The SWAB calculation
 - The Data Operator (mud logger) was not aware that, on the next page in the drilling program, a detailed plot of the reservoir section was presented



After the incident the swab calculation was performed with the maximum expected pore pressure

SWAB TRI	PPING S	PEED C	ALCULATIONS		
	РООН				1
DATE:	28-mar-10				
STRING:	BHA #7				
TOTAL DEPTH:	3506mMD	2625mTVD			
MUDWEIGHT:	1.3	SG			
LAST FIT:	1.61	SG			
LAST Pore P:	1.24	SG			
Max ECD	1.41	SG			
Heave effect :	0.02	m/sec			
BIT DEPTH	EMW	1.3	Running spe	ed w/ heave	
meters	m/sec	sec/std	m/sec	sec/std	m/hr
3500	0.1	290	0.08	363	288
3200	0.12	242	0.10	290	360
3000	0.15	193	0.13	223	468
2700	0.18	161	0.16	181	576
2000	0.21	138	0.19	153	684
1000	0.3	97	0.28	104	1008

Would you have queationed this swab calculation?



After the incident the swab calculation was performed with the maximum expected pore pressure

SWAB TRI	PPING S	SPEED C	ALCULATIONS		
	РООН				1
DATE:	28-mar-10				
STRING:	BHA #7				
TOTAL DEPTH:	3506mMD	2625mTVD			
MUDWEIGHT:	1.3	SG			
LAST FIT:	1.61	SG			
LAST Pore P:	1.24	SG			
Max ECD	1.41	SG			
Heave effect :	0.02	m/sec			
BIT DEPTH	EMW	1.3	Running spe	ed w/ heave	
meters	m/sec	sec/std	m/sec	sec/std	m/hr
3500	0.1	290	0.08	363	288
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2700	0.18	161	0.16	181	576
2000	0.21	138	0.19	153	684
1000	0.3	97	0.28	104	1008

Would you have reacted on this swab calculation?

- Consider to pump out of hole due to very low pulling speed?



After the incident the swab calculation was performed with the maximum expected pore pressure

SWAB TRI	PPING S	SPEED C	ALCULATIONS		
	РООН				1
DATE:	28-mar-10				
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- Consider to pump out of hole due to very low pulling speed?

- Increase mud weight before POOH?



After the incident the swab calculation was performed with the maximum expected pore pressure

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	РООН				1	V
DATE:	28-mar-10					
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LAST FIT:	1.61	SG				
LAST Pore P:	1.24	SG				-
Max ECD	1.41	SG				
Heave effect :	0.02	m/sec				d
BIT DEPTH	EMW	1.3	Running spe	ed w/ heave		
meters	m/sec	sec/std	m/sec	sec/std	m/hr	-
3500	0.1	290	0.08	363	288	Р
3200	0.12	242	0.10	290	360	L .
3000	0.15	193	0.13	223	468	
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1000	0.3	97	0.28	104	1008	

Would you have reacted on this swab calculation?

- Consider to pump out of hole due to very low pulling speed?

- Increase mud weight before POOH?

Actual PP in formation was measured in 6" hole section: 1.28 sg



Summary

The well control incident occurred mainly due to:

•Hydrocarbons were swabbed due to high tripping speed

- ✓ The input parameters to the swab calculation were wrong
- ✓No QC of the swab calculation was performed
- •The PP was higher than the maximum estimated value
 - ✓ Expected: 1.16 sg / maximum expected: 1.24 sg / measured: 1.28 sg
- •No flow checks were performed inside 9 5/8" casing shoe and before the BHA was pulled through the BOP
- •The trip sheet indicating gain was not reacted on



Recommendations – Planning phase onshore

•The PP estimates for the reservoir section should be presented in a table

•A comment should be entered on the PP chart stating that a detailed PP chart/table for the reservoir section is available

•The risk matrix for sections with possible permeable zones should state the risk and consequences related to surge/swab



Recommendations – Planning phase onshore/offshore

•Flow checks should be included in the detailed operating procedure (DOP):

≻At TD

➤Inside last casing shoe

➢Before BHA is pulled through BOP

✓ Length of flow checks:

Minimum 10 minutes (HPHT: 30 minutes)

•In section- and DOP meetings, well control issues should be discussed and related risks and actions evaluated



Recommendations – Operational phase offshore

•The Wellsite Geologist should at all times know the expected and maximum expected PP in the ongoing hole section

•The Data Operator (mud logger) should verify the input parameters to the swab calculation with the Wellsite Geologist and the Drilling Supervisor

•The swab calculation should be quality controlled by the Tool pusher and Well site Geologist. The Drilling Supervisor should sign out the calculation results

•Prior to tripping, trip sheet tolerances, alarm settings, shut-in procedure and other criteria's shall be agreed between the Data Operator (mud logger), Driller, Tool pusher and Drilling Supervisor

•If the trip sheet indicate well instability, a flow check shall be performed and the Tool pusher and Drilling Supervisor notified. The driller should line up for closing the well.

•If a flow check indicate instability, the well shall be shut in as soon as possible and the Tool pusher and Drilling Supervisor notified

•Extended length of flow checks should be considered based on well geometry, drilling fluid, expected overbalance and other operational considerations



Thank you

