

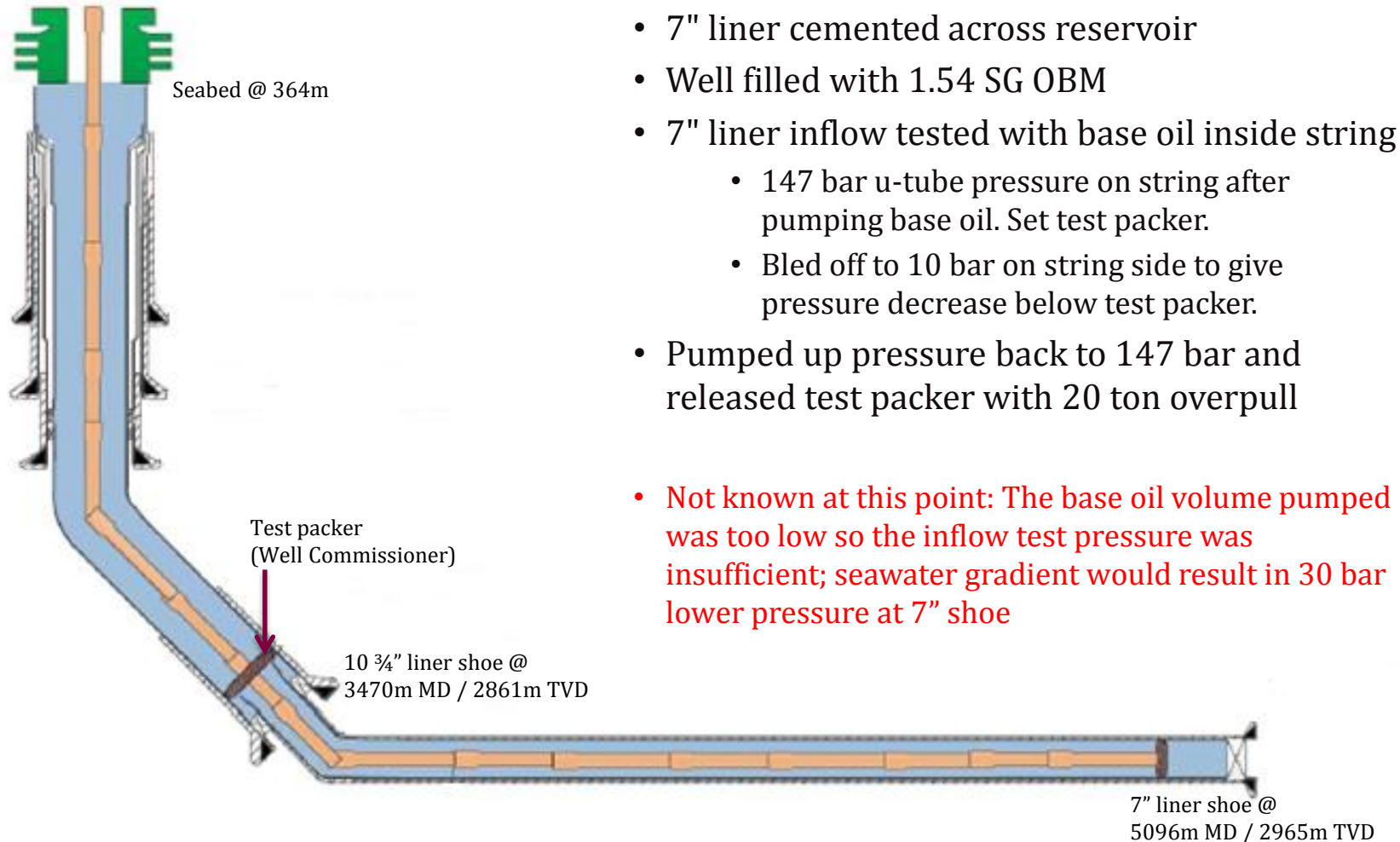


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# "Sharing To Be Better"

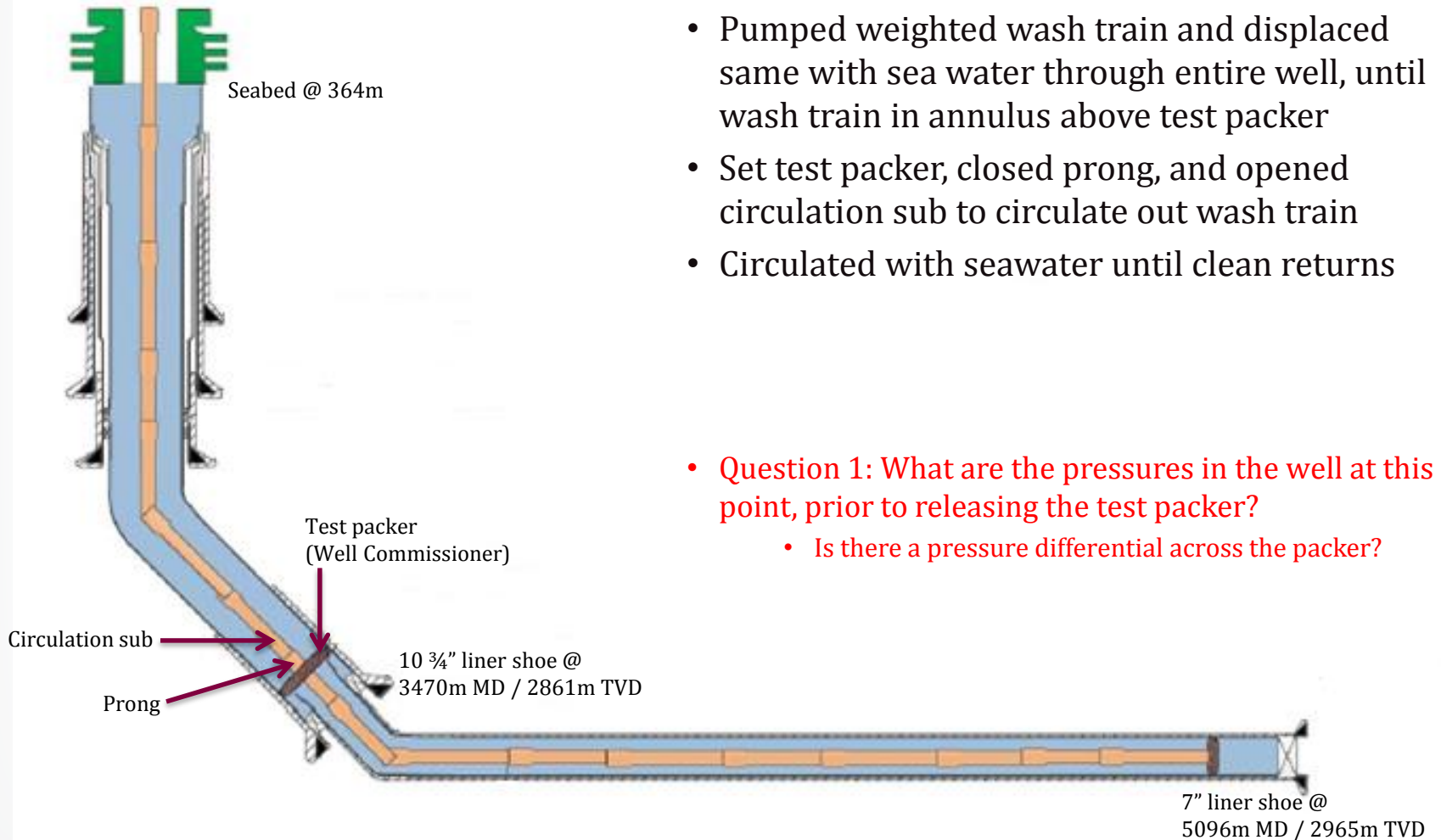
Influx through failed cement in shoetrack during completion operations

# Well status – completion operations

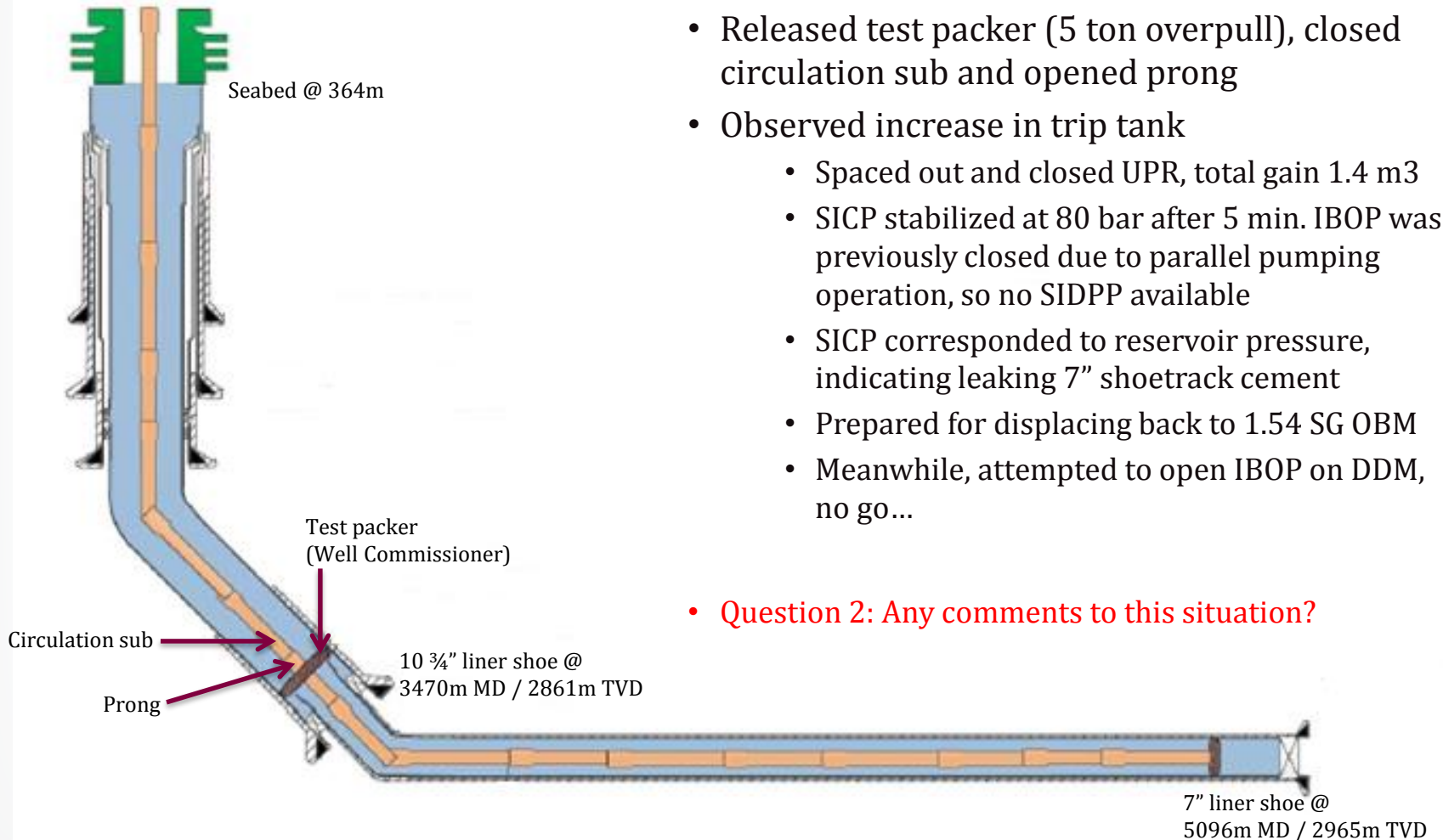


- 7" liner cemented across reservoir
- Well filled with 1.54 SG OBM
- 7" liner inflow tested with base oil inside string
  - 147 bar u-tube pressure on string after pumping base oil. Set test packer.
  - Bled off to 10 bar on string side to give pressure decrease below test packer.
- Pumped up pressure back to 147 bar and released test packer with 20 ton overpull
- **Not known at this point: The base oil volume pumped was too low so the inflow test pressure was insufficient; seawater gradient would result in 30 bar lower pressure at 7" shoe**

# Washing and displacement to sea water

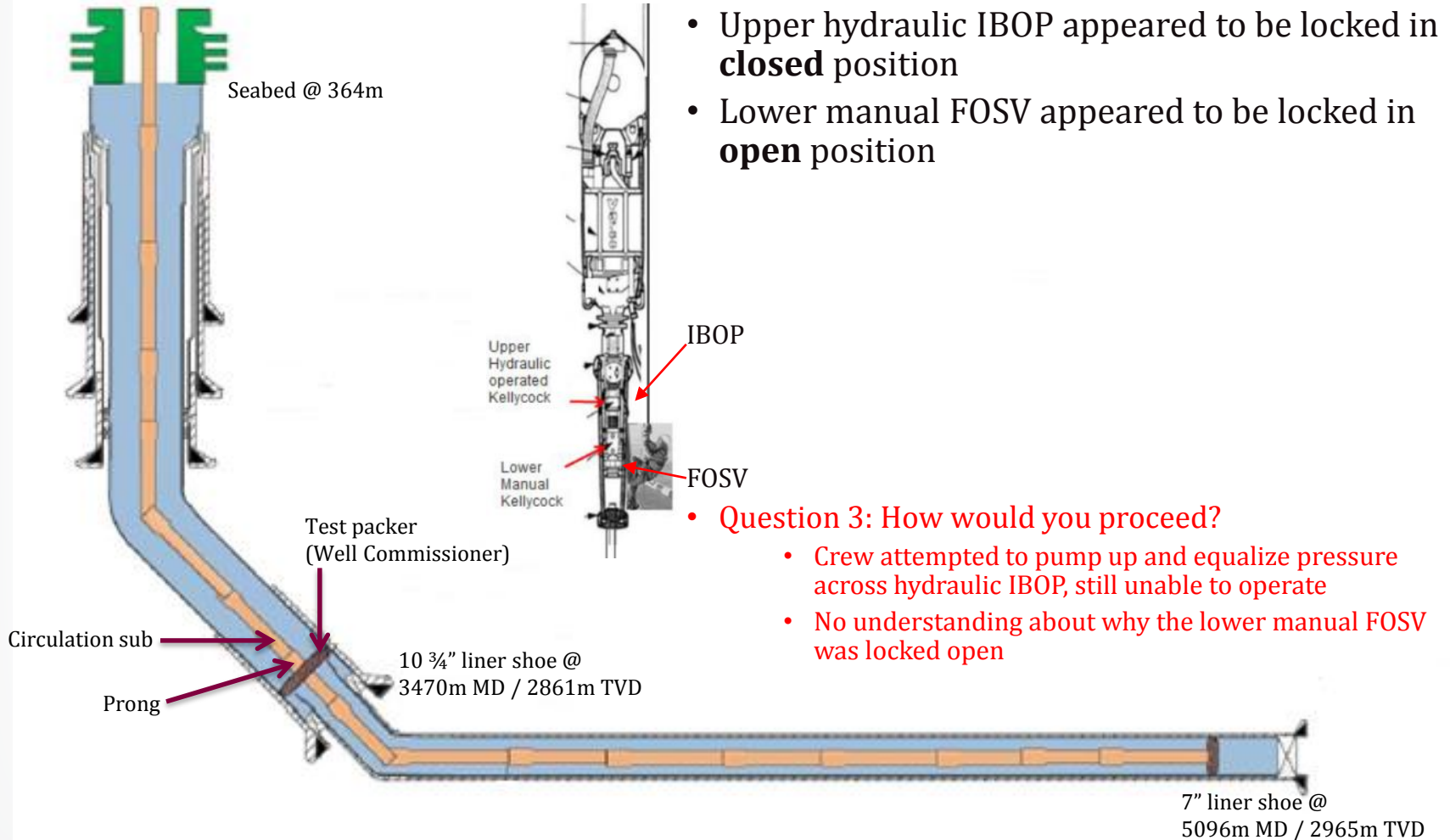


# Prepare for displacement to heavy brine



- Released test packer (5 ton overpull), closed circulation sub and opened prong
- Observed increase in trip tank
  - Spaced out and closed UPR, total gain 1.4 m<sup>3</sup>
  - SICP stabilized at 80 bar after 5 min. IBOP was previously closed due to parallel pumping operation, so no SIDPP available
  - SICP corresponded to reservoir pressure, indicating leaking 7" shoetrack cement
  - Prepared for displacing back to 1.54 SG OBM
  - Meanwhile, attempted to open IBOP on DDM, no go...
- **Question 2: Any comments to this situation?**

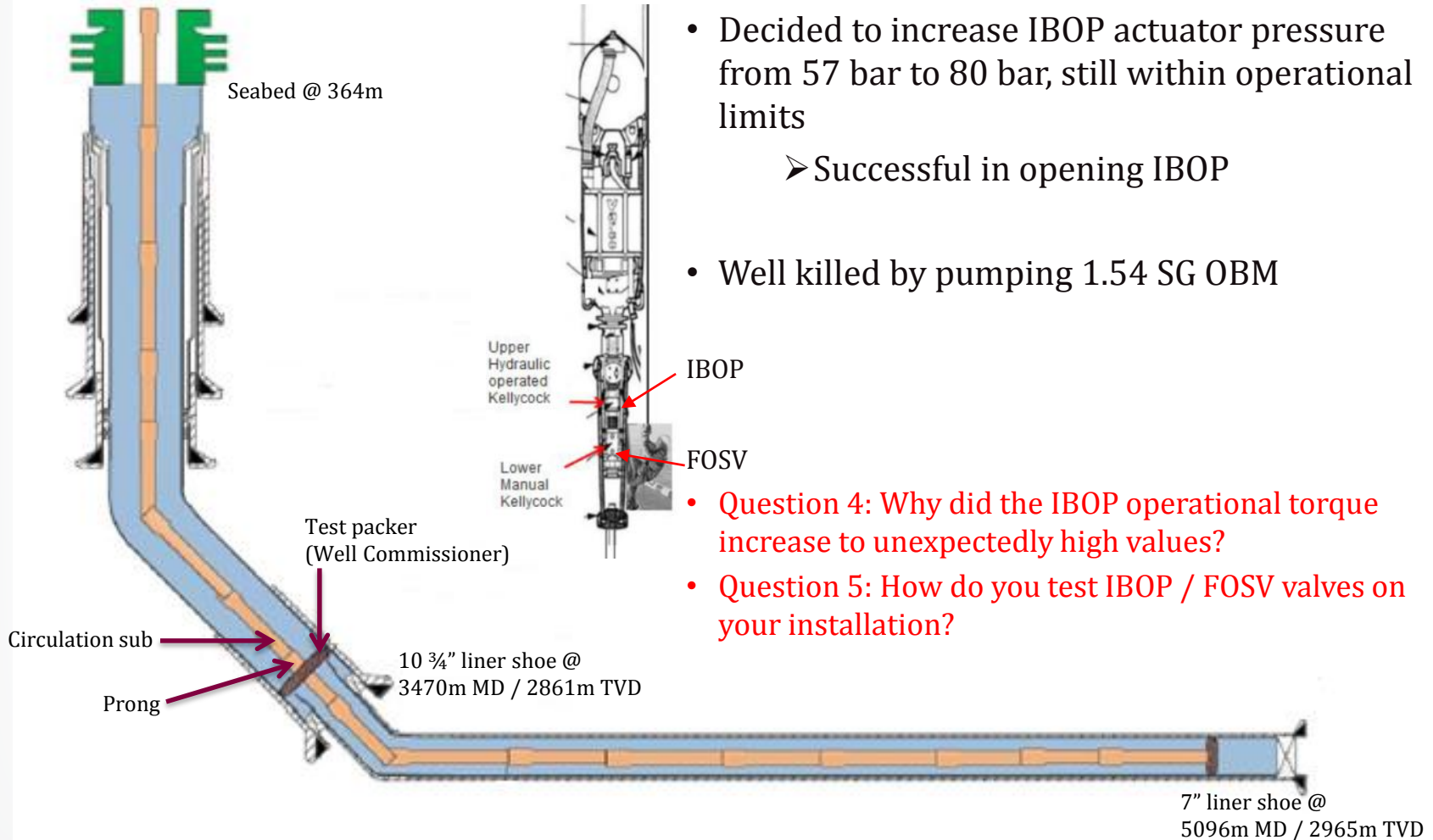
# Well shut in with 80 bar SICP



- Upper hydraulic IBOP appeared to be locked in **closed** position
- Lower manual FOSV appeared to be locked in **open** position

- **Question 3: How would you proceed?**
  - Crew attempted to pump up and equalize pressure across hydraulic IBOP, still unable to operate
  - No understanding about why the lower manual FOSV was locked open

# Handling the situation



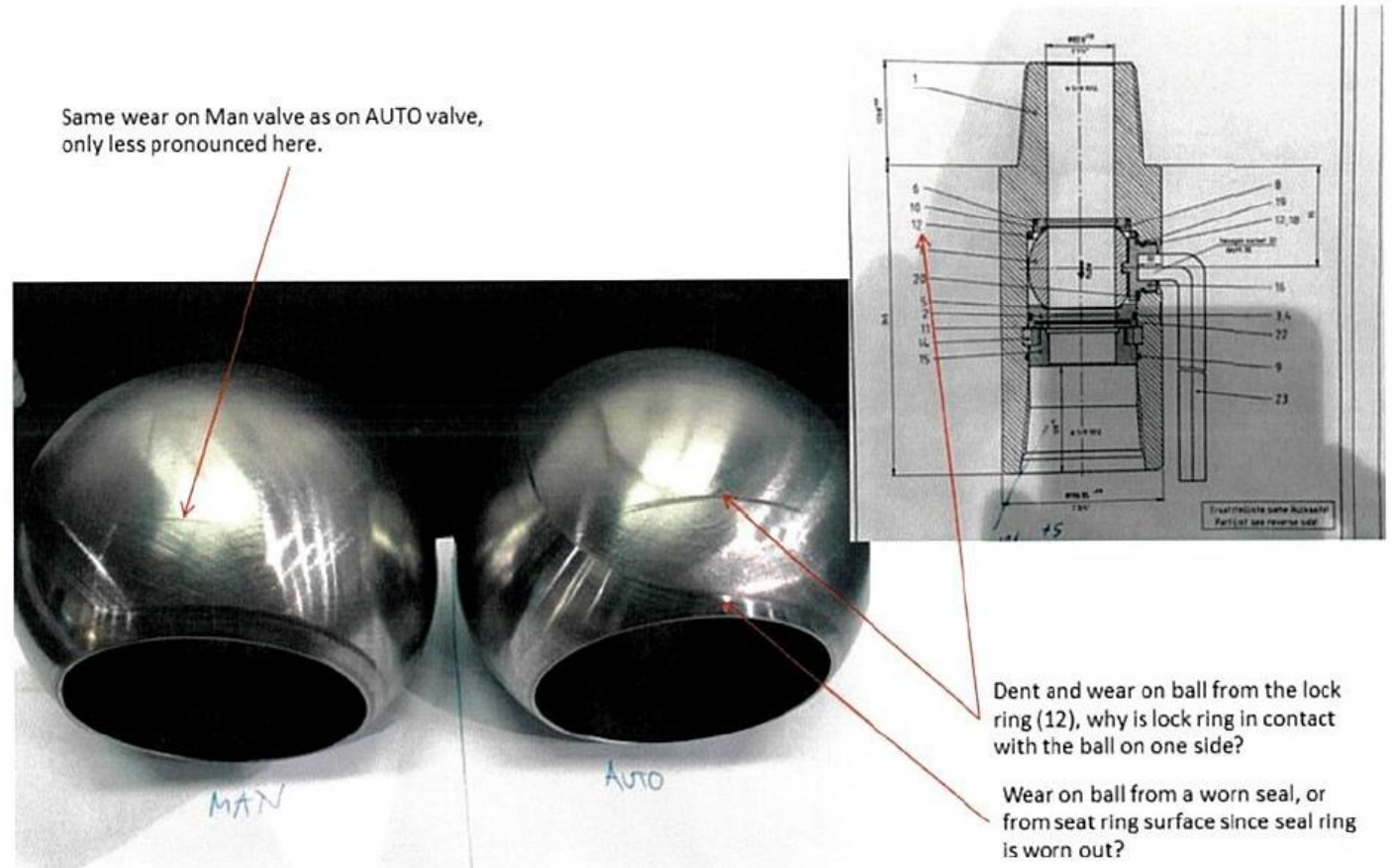
- Decided to increase IBOP actuator pressure from 57 bar to 80 bar, still within operational limits
  - Successful in opening IBOP
- Well killed by pumping 1.54 SG OBM
- Question 4: Why did the IBOP operational torque increase to unexpectedly high values?
- Question 5: How do you test IBOP / FOSV valves on your installation?



# IBOP and FOSV investigation findings

## Managed to reproduce the high operational torque in workshop

- Wear marks on ball indicating contact between ball and lock ring above



- Question 6: Do you have a tracking system for IBOP and manual FOSV?



# IBOP and FOSV investigation findings

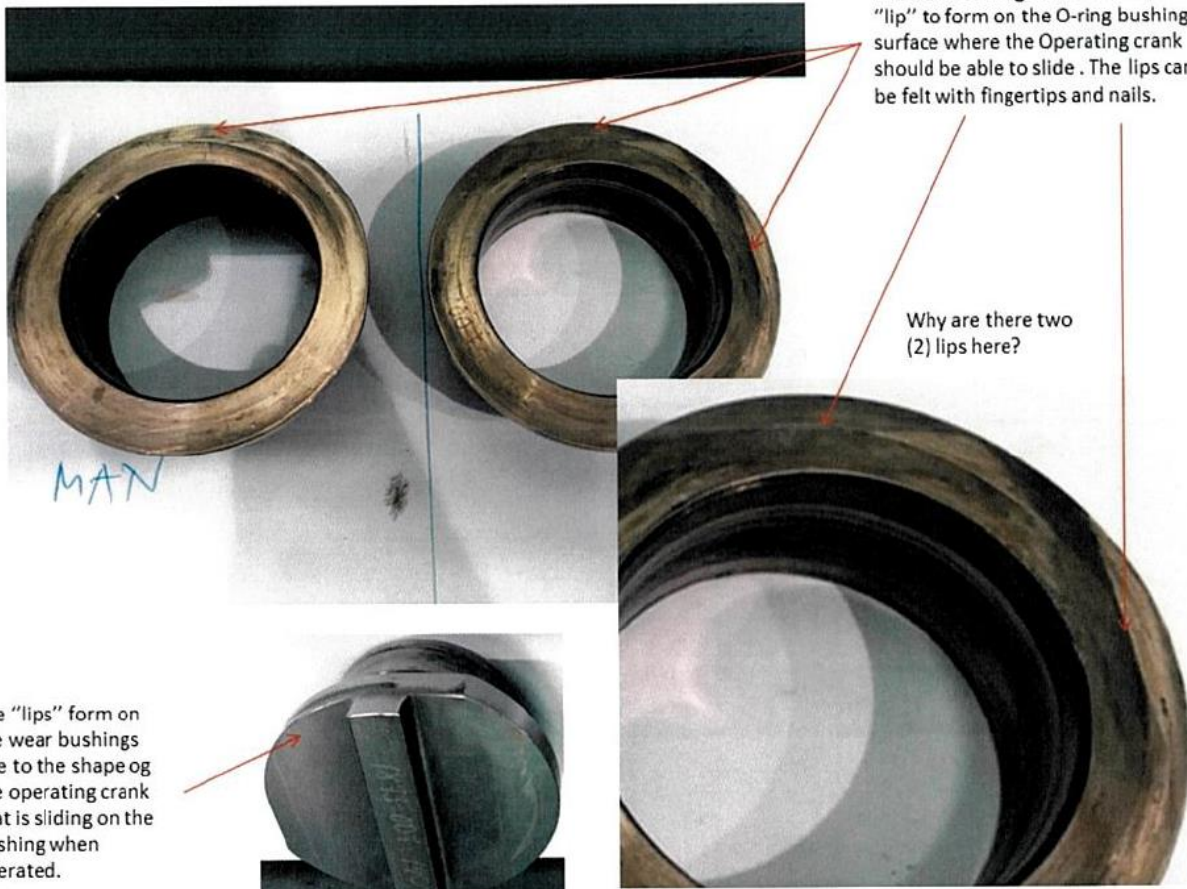
Wear on bushings have caused a "lip" to form on the O-ring bushing surface where the Operating crank should be able to slide. The lips can be felt with fingertips and nails.

Why are there two (2) lips here?

**Managed to reproduce the high operational torque in workshop**

- 2 wear lips on bushing surface indicating possible rotation of bushing vs. crank
- No maintenance history found. Function testing under pressure not implemented.

The "lips" form on the wear bushings due to the shape of the operating crank that is sliding on the bushing when operated.



- Question 7: How do you inspect the Top Drive installed automatic and manual valves if done offshore?

# Learnings and recommendations

- Inflow test pressure was insufficient, due to insufficient detail in operational procedure
  - Include both volume and expected pressure in operational procedure
  - After inflow test, the well shall still be monitored
- No tracking system for valve maintenance
  - Notify contractors of expectation
- Valves had significant wear while still passing pressure tests
  - Suggest review of existing FOSV's and stab-in kelly-cocks
  - Recommend to use improved valve designs, available on the market
  - Establish routines for change-out based on operational history
- Weakness in valve design was not uncovered during routine testing without pressure on valve when operating it
  - Acquire vendor operational torque values to operate valve. To be available on drill floor.
  - Discuss with vendor about routinely test-operating the valve under pressure.